## Revision and Errata List— March 2021 AISC Steel Construction Manual, 15<sup>th</sup> Edition

The following list represents corrections to the Third Printing of the AISC *Steel Construction Manual*, 15th Edition. These corrections are incorporated in the Fourth Printing dated March 2021.

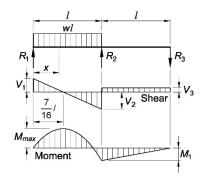
## Page(s) Item

3-207 Replace the top figure in Table 3-22c with the following (right figure, fourth row, middle two terms, denominator revised to 38).

Uniform Load	
Moment in terms of $wl^2$	Shear in terms of wl
125 +.08 +.025 +.08	<u>ola <u>5t5</u> <u>3to</u></u>
	<u>014 815 518 410</u> 10 10 10 10
+.077 +.036 +.036 +.077 +.078 -107071107 +.078	<u>0 11 17 15 13 13 15 17 11 0</u> 28 28 28 28 28 28
+.078105079079105 +.078	0 <mark>115 23120 18119 19118 20123 1510</mark> 38 38 38 38 38 38 38 38
+.078106077086077106 +.078	0141 63155 49151 53153 51149 55163 4110 104 104 104 104 104 104 104 104
106077085085077106	<u>0156 86175 67170 72171 71172 70167 75186 5610</u> 142 142 142 142 142 142 142 142 142 142

3-218

Replace the figure for Case 29 with the following (direction of  $R_3$  arrow reversed):



4-106 thru 4-131	Add the following to the Table 4-7 footer:
	Note: Interpolation between $L = 0$ ft and 10 ft for the Y-Y axis may produce an incorrect result.
4-132 thru 4-138	Add the following to the Table 4-7 footer:
	Note: Interpolation between $L = 0$ ft and 4 ft for the Y-Y axis may produce an incorrect result.
7-85 to 7-86	Revise Table 7-19 as shown in "15th Edition Manual Errata - 3rd Printing_ATT 1"

8-15 Revise Equation 8-16 as follows  $(2e_x^2 \text{ revised to } 2e_x)$ :

$$l_a = \frac{\sqrt{4e_x^2 + l_w^2 \tan^2 \theta} - 2e_x}{\tan \theta}$$
(8-16)

8-16 Revise Equation 8-17 as follows  $(2e_x^2 \text{ revised to } 2e_x)$ :

$$f_a = \frac{N}{l_a} = \frac{N \tan \theta}{\sqrt{4e_x^2 + l_w^2 \tan^2 \theta} - 2e_x}$$
(8-17)

Revise Equation 8-18 as follows (*M* revised to 4*M*):

$$f_b = \frac{4M}{l_w^2 - l_a^2} \tag{8-18}$$

9-17 Revise Equation 9-35 as follows ( $\rho$  replaced with  $\eta$ ):

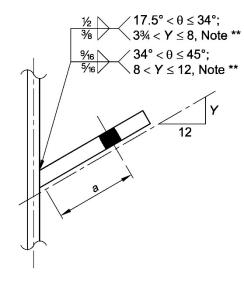
$$M_n = \frac{t^2 F_y}{4} \left( \frac{4\sqrt{2abcT\eta} + L\eta}{2ab} \right)$$
(9-35)

Revise Equation 9-36 to 9-36a and add new Equation 9-36b:

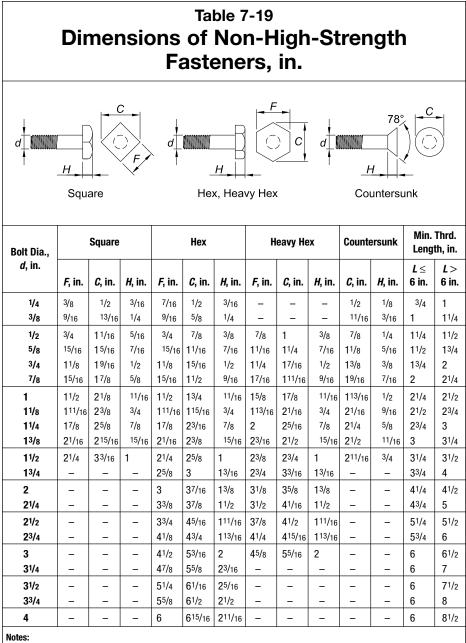
$$\rho = 2ab + ac + bc \tag{9-36a}$$

$$\eta = 4ab + ac + bc \tag{9-36b}$$

10-163 Replace the "For  $17.5^\circ < \theta \le 45^\circ$  from Perpendicular" figure with the following (shear plate is now beveled):



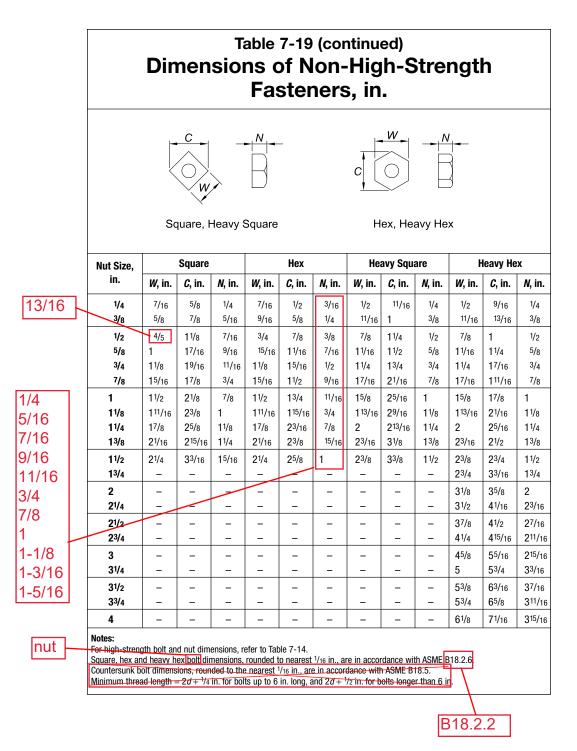
- 16.1-167 In Section M2.1, replace the second sentence with "The temperature of heated areas shall not exceed 1,100°F (590°C) for ASTM A514/A514M steel nor 1,200°F (650°C) for other steels."
- 16.1-358 At the end of the first sentence on the page, the expression " $P \ge 1.5P_y$ " is revised to " $P \ge 0.15P_y$ "



For high-strength bolt and nut dimensions, refer to Table 7-14. Square, hex and heavy hex bolt dimensions, rounded to nearest 1/16 in., are in accordance with ASME B18.2.6 Countersunk bolt dimensions, rounded to the nearest <sup>1</sup>/<sub>16</sub> in., are in accordance with ASME B18.5. Minimum thread length =  $2d + \frac{1}{4}$  in. for bolts up to 6 in. long, and  $2d + \frac{1}{2}$  in. for bolts longer than 6 in.

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B18.2.1



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