

# Joining Forces



## AISC's Steel Design Specifications Merge in 2005

By Cynthia J. Duncan

**T**he new 2005 unified design specification for structural steel buildings will combine individual ASD and LRFD specifications with one document. The document is on schedule for completion in early 2005, and will replace the two existing AISC building design specifications: the 1989 *Specification for Structural Steel Buildings-Allowable Stress Design (ASD) and Plastic Design* and the 1999 *Load and Resistance Factor Design Specification (LRFD) for Structural Steel Buildings*.

It also will replace the two AISC special-member design specifications, the 2000 *Load and Resistance Factor Design Specification for Steel Hollow Structural Sections*, and the 2000 *Load and Resistance Factor Design Specification for Single-Angle Members*. This means that all HSS and single-angle member and connection-design provisions will be incorporated into the 2005 specification. The organization of the combined specifications is very similar to the existing individual specifications to ease the transition to the new document.

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### It's No Longer ASD vs. LRFD

By Jason Ericksen, Senior Advisor, Steel Solutions Center

In 2005, AISC will issue a new specification for structural steel buildings that will supersede both of the existing specifications (Allowable Stress Design and Load & Resistance Factor Design). This new unified specification will reflect the current state of engineering knowledge and allow engineers to use either factored loads or service loads in their calculations. As Louis Geschwindner, AISC Vice President of Engineering and Research, said: "There is no intention to phase out ASD. As long as ASCE 7 has service-load combinations, there will be ASD design procedures."

Rightly or wrongly, when the *LRFD Specification* was introduced in 1986, it was widely viewed as a difficult design methodology foisted on the industry by the academic community. The new unified specification should avoid those difficulties if for no other reason than that more than two-thirds of the current Committee on Specifications, including the current chair, comes from either the design community or fabrication industry. According to Geschwindner, the new specification:

- is practice oriented.
- provides economical designs.

- meets the engineering requirement of providing safe designs with predictable behavior and response.

A key reason that ASD often was viewed as easier than LRFD (besides the obvious factors of familiarity and resistance to change) is that the current *ASD Specification* essentially is unchanged since 1961. If AISC had never introduced LRFD but had instead simply updated ASD design procedures, then ASD would look a lot like LRFD. In discussing this issue, Geschwindner often relates the story of the designer who stated that "If I have to do leaning columns in LRFD then I'm going to use ASD." But steel doesn't know whether you're using LRFD or ASD—and there are still leaning columns!

The limit states for both methods are the same—and always have been. And you can easily look at using stress as opposed to member strength: If you follow the math, allowable bending stress is  $(Z/S) * 0.6F_y$ . If  $(Z/S)$  is taken as 1.1, as was done in the *ASD Specification*, then the allowable bending stress would be  $0.66F_y$  as it is in the 1989 *ASD Specification* and has been since 1961. And a designer could certainly continue to use that value.

| Table 4-2.<br>W-Shapes<br>Available Strength in Axial<br>Compression, kips   |       |   |       |      |       |                  |       |                  |       |      |       |      |      |
|--|-------|---|-------|------|-------|------------------|-------|------------------|-------|------|-------|------|------|
| $F_y = 50$ ksi<br>$P_n = F_{cr} A_g$<br>$\Omega_c = 1.67$<br>$\phi_c = 0.90$ |       | $P_n / \Omega_c$ (ASD)<br>$\phi_c P_n$ (LRFD) |       |      |       |                  |       |                  |       |      |       |      |      |
| Shape  |       | W14x  |       |      |       |                  |       |                  |       |      |       |      |      |
| Wt/ft  |       | 120   |       | 109  |       | 99 <sup>††</sup> |       | 90 <sup>††</sup> |       | 82   |       | 74   |      |
| Design   |       | ASD   | LRFD  | ASD  | LRFD  | ASD              | LRFD  | ASD              | LRFD  | ASD  | LRFD  | ASD  | LRFD |
| Effective length KL (ft) with respect to least radius of gyration r          | 0     | 1059  | 1588  | 960  | 1440  | 875              | 1313  | 798              | 1196  | 720  | 1080  | 654  | 982  |
|  | 6     | 1031  | 1546  | 932  | 1398  | 847              | 1271  | 776              | 1165  | 677  | 1015  | 615  | 922  |
|  | 7     | 1024  | 1535  | 925  | 1387  | 840              | 1260  | 762              | 1144  | 662  | 993   | 601  | 902  |
|  | 8     | 1009  | 1514  | 918  | 1376  | 833              | 1249  | 755              | 1133  | 645  | 968   | 586  | 879  |
|  | 9     | 995   | 1493  | 904  | 1355  | 819              | 1228  | 748              | 1122  | 627  | 940   | 570  | 854  |
|  | 10    | 981   | 1472  | 889  | 1334  | 812              | 1218  | 734              | 1101  | 607  | 911   | 551  | 827  |
|  | 11    | 967   | 1451  | 875  | 1313  | 798              | 1196  | 727              | 1091  | 585  | 882   | 532  | 797  |
|  | 12    | 953   | 1429  | 861  | 1292  | 784              | 1175  | 713              | 1069  | 563  | 853   | 511  | 767  |
|  | 13    | 932   | 1398  | 847  | 1271  | 769              | 1154  | 698              | 1043  | 539  | 823   | 490  | 735  |
|  | 14    | 911   | 1366  | 826  | 1239  | 748              | 1122  | 681              | 1021  | 517  | 792   | 467  | 701  |
|  | 15    | 896   | 1345  | 812  | 1218  | 734              | 1101  | 665              | 1000  | 495  | 761   | 445  | 667  |
|  | 16    | 875   | 1313  | 791  | 1186  | 720              | 1079  | 649              | 979   | 474  | 730   | 422  | 633  |
|  | 17    | 854   | 1281  | 769  | 1154  | 700              | 1043  | 637              | 955   | 453  | 699   | 399  | 598  |
|  | 18    | 833   | 1249  | 748  | 1122  | 681              | 1021  | 620              | 930   | 434  | 670   | 376  | 563  |
|  | 19    | 805   | 1207  | 719  | 1079  | 662              | 993   | 602              | 903   | 388  | 582   | 352  | 528  |
|  | 20    | 784   | 1175  | 700  | 1043  | 643              | 965   | 584              | 877   | 363  | 544   | 330  | 494  |
|  | 22    | 771   | 1154  | 666  | 998   | 603              | 904   | 548              | 822   | 314  | 471   | 286  | 429  |
|  | 24    | 768   | 1151  | 620  | 931   | 562              | 843   | 510              | 766   | 268  | 402   | 244  | 365  |
|  | 26    | 767   | 1149  | 575  | 863   | 520              | 780   | 473              | 709   | 229  | 343   | 208  | 311  |
|  | 28    | 767   | 1149  | 530  | 795   | 479              | 719   | 435              | 652   | 197  | 295   | 179  | 268  |
| 30   | 767   | 1149  | 486   | 728  | 438   | 658              | 398   | 597              | 172   | 257  | 156   | 234  |      |
| 32   | 490   | 735   | 443   | 664  | 399   | 598              | 361   | 542              | 151   | 227  | 137   | 205  |      |
| 34   | 443   | 665   | 400   | 600  | 361   | 541              | 327   | 490              | 133   | 200  | 121   | 182  |      |
| 36   | 399   | 598   | 359   | 539  | 323   | 485              | 293   | 439              | 119   | 179  | 108   | 162  |      |
| 38   | 358   | 537   | 323   | 484  | 290   | 435              | 263   | 394              | 107   | 160  | 97.4  | 146  |      |
| 40   | 323   | 484   | 291   | 436  | 262   | 393              | 237   | 356              | 96.7  | 145  | 87.5  | 131  |      |
| Properties   |       |   |       |      |       |                  |       |                  |       |      |       |      |      |
| $P_{wo}$ , kips  | 151   | 227   | 128   | 192  | 111   | 167              | 96    | 144              | 123   | 185  | 103   | 155  |      |
| $P_{wi}$ , kips/in.  | 19.7  | 29.5  | 17.5  | 26.3 | 16.2  | 24.3             | 14.7  | 22.0             | 17.0  | 25.5 | 15.0  | 22.5 |      |
| $P_{wb}$ , kips  | 331   | 497   | 233   | 349  | 184   | 275              | 137   | 205              | 213   | 320  | 226   | 339  |      |
| $P_{fb}$ , kips  | 176   | 264   | 147   | 220  | 121   | 181              | 100   | 150              | 145   | 218  | 154   | 231  |      |
| $L_p$ , ft   | 13.2  |   | 13.2  |      | 13.5  |                  | 15.1  |                  | 8.76  |      | 8.76  |      |      |
| $L_r$ , ft   | 46.2  |   | 43.2  |      | 40.6  |                  | 38.4  |                  | 29.5  |      | 27.9  |      |      |
| $A_g$ , in. <sup>2</sup>   | 35.3  |   | 32.0  |      | 29.1  |                  | 26.5  |                  | 24.0  |      | 21.8  |      |      |
| $I_x$ , in. <sup>4</sup>   | 1380  |   | 1240  |      | 1110  |                  | 999   |                  | 881   |      | 795   |      |      |
| $I_y$ , in. <sup>4</sup>   | 495   |   | 447   |      | 402   |                  | 362   |                  | 148   |      | 134   |      |      |
| $r_y$ , in.  | 3.74  |   | 3.73  |      | 3.71  |                  | 3.70  |                  | 2.48  |      | 2.48  |      |      |
| Ratio $r_x/r_y$  | 1.67  |   | 1.67  |      | 1.66  |                  | 1.66  |                  | 2.44  |      | 2.44  |      |      |
| $P_{ex}(KL)^2/10^4$  | 39500 |   | 35500 |      | 31800 |                  | 28600 |                  | 25200 |      | 22800 |      |      |
| $P_{ey}(KL)^2/10^4$  | 14200 |   | 12800 |      | 11500 |                  | 10400 |                  | 4240  |      | 3840  |      |      |

<sup>††</sup> Flanges are non-compact; See AISC Specification Section B4.

Example of column table for the next manual, using draft provisions of the 2005 Specification. ASD design values will be shaded in green, and LRFD design values will be shown in blue. Member design tables are for  $F_y = 50$  ksi.

### Expanded Scope

The new unified format of the 2005 specification is the most visible change, incorporating both ASD and LRFD methods into one specification. The document begins with a substantial revision: an expanded scope in Chapter A will affect the applicability of the entire document by stating that the specification sets forth criteria for the "design of structural steel buildings and other structures." Chapter B provides a roadmap to help the user

locate specific provisions in the specification. Chapter C handles the stability provisions of the overall structure, and incorporates new analysis provisions, including a direct-analysis method using notional loads and  $K = 1$ .

### Member Design

Chapters D through I cover member-design provisions, and Chapter J covers connection-design provisions. Chapter D, "Design of Members for Tension," will

include simplified shear-lag criteria for determining the effective area in a new tabulated format. The other remaining member-design chapters contain several revisions. Chapter F, "Design of Members for Flexure," has expanded in length with the addition of hollow structural section and single-angle provisions. However, it is helpful to note that the user need not go past Section F2 if designing the typical, compact wide-flange shape.

Other notable revisions to member design are in Chapter I, where "Design of Composite Members" has been reorganized and updated extensively to reflect recent research, higher-strength materials, and consistency with ACI 318. The usual bolt, weld, and general connection-design provisions remain in Chapter J, and a new Chapter K addresses only HSS and box-member connection-design provisions. The concentrated-force provisions have been relocated to Chapter J. Some revisions in Chapter J include new block shear rupture criteria, improved details for weld-access holes, and revised slip-strength calculations for slip-critical connections.

### User Notes Added

Other important features of the new specification are found in the appendices and "User Notes." The appendices are intended to contain less frequently used criteria, including "Design for Fatigue, Evaluation and Repair," and a new appendix on "Structural Design for Fire Conditions." The latter provides a more performance-oriented approach to design for fire than the traditional prescriptive methods used in the building code. The "User Notes" are brief commentaries interspersed throughout the text that supplement the historical "Commentary" that follows the specification. They provide concise, practical guidance to assist the user when applying the provisions.

### Availability

The final, ANSI-accredited AISC Specification for Structural Steel Buildings will be introduced in 2005 in conjunction with a completely updated Manual of Steel Construction. The Manual will provide the discussion, tables, and design aids that the user will need to make the most of the new specification. ★

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